

EFFECT OF DEPOSIT COMPOSITION AND QUALITY ON CORROSION OF ELECTROLESS NICKEL COATINGS

The corrosion resistance of an Electroless Nickel coating is a function of two factors, alloy passivity and deposit quality. Passivity is an electrochemical term which describes a metal's or alloy's loss of chemical reactivity (its reduced corrosion) under specific environmental conditions. This is normally due to the formation of a protective film only a few atoms thick, on the surface of the metal.

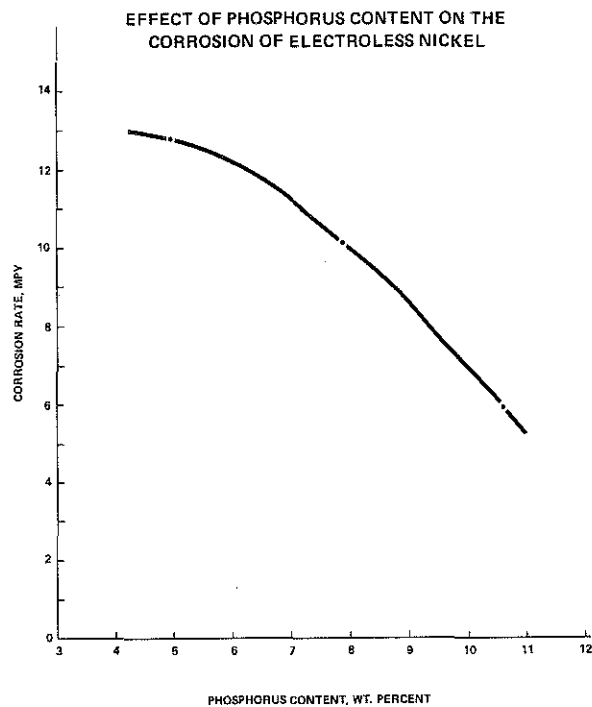
Whether a metal is passive, and the degree of its passivity, is a function of the metal's composition and its environment. For example, Type 300 stainless steels are passive and do not appreciably corrode in oxidizing media such as nitric acid or aerated seawater. If, however, these stainless steels are placed in a reducing environment, such as hydrochloric acid or deaerated seawater, they will be rapidly attacked.

ALLOY PASSIVITY

Most Electroless Nickel coatings display natural passivity and are very resistant to reducing, neutral, and most oxidizing environments. Their degree of passivity, however, is greatly affected by their phosphorus content; higher phosphorus alloys are more easily passivated and are more corrosion resistant than those with lower phosphorus concentration. This is illustrated by Figure 1, which compares the corrosion experienced by Electroless Nickel coatings containing $4\frac{1}{2}$ to $10\frac{1}{2}$ percent phosphorus in aerated citric acid at 122°F (50°C)¹.

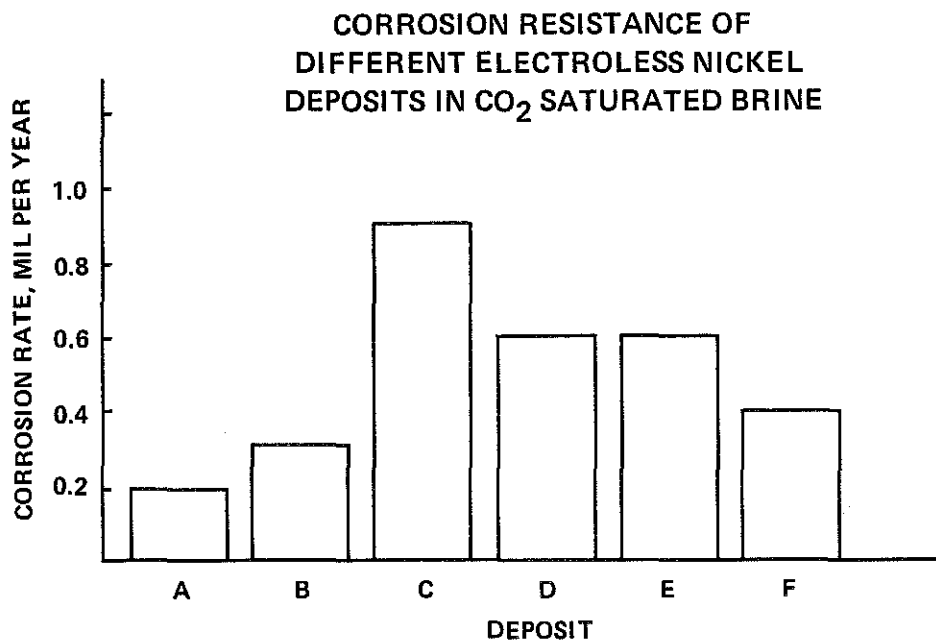
In this test, corrosion of the $10\frac{1}{2}$ percent phosphorus Electroless Nickel was only about one half of that of lower phosphorus coatings. Unfortunately, most of the Electroless Nickel sold today is of the latter type, and typically contains only 7 to 9 percent phosphorus.

FIGURE 1



Often, the contaminants present in the coating are even more important to an Electroless Nickel's corrosion resistance. Most coatings are applied from baths stabilized with lead, cadmium or sulfur. Codeposition of these elements with an Electroless Nickel coating will cause a severe reduction in its passivity and corrosion resistance. This is illustrated by Figure 2, which shows the results of corrosion tests with 6 different commercial Electroless Nickel deposits in CO₂ saturated, 3½ percent salt brine at 200°F (95°C)².

FIGURE 2



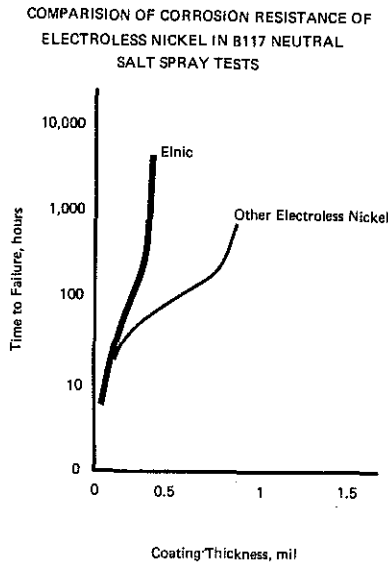
These tests showed hugh differences between the coatings. The deposit (A) had a loss of 0.2 mpy (5 $\mu\text{m}/\text{y}$) while that of the other deposits was 50 to 450 percent higher. Similar tests in 10 percent HCl at ambient temperature showed even larger differences; P ; and Deposit B had corrosion rates of 0.6 and 0.8 mpy (15 and 20 $\mu\text{m}/\text{y}$) respectively, while Deposits C through F were 8 to 26 mpy (200 to 600 $\mu\text{m}/\text{y}$).

The primary differences between these deposits was not their phosphorus content, but rather their baths' stabilizing system. ELNIC is applied from an organically stabilized bath, and contains only trace amounts of contaminants. Deposits B, C, D, E and F, however, were found to contain 500 to 1500 ppm of either lead, cadmium, tin or sulfur.

DEPOSIT QUALITY

The second factor controlling an Electroless Nickel coating's corrosion resistance is the deposit's quality. Electroless Nickel is free of defects. The coating is continuous. Unfortunately, the structure of most other coatings is not like this; instead they consist of many small islands of Electroless Nickel separated by cracks or pores. Since Electroless Nickel is a barrier coating and protects the underlying metal by sealing it off from the environment, these coatings offer only limited protection. Each crack and pore serves as a tunnel to allow the corrodent through the coating and to the substrate. This effect is illustrated by Figure 3, which compares the resistance of Electroless Nickels to an ASTM B117 neutral salt spray test.

FIGURE 3



While a 0.4 mil thickness of Electroless Nickel will provide 1000 hours of salt spray resistance, with other coatings thicknesses greater than one mil may be needed to provide the same level of protection.

Defects form in most Electroless Nickel coatings for two reasons. First, the level of internal stress of low phosphorus coatings is quite high. Electroless Nickel coatings, containing only 7 to 9 percent phosphorus, develop internal tensile stresses of 3000 to 5000 psi (20 to 35 MPa). These coatings are like rubber bands tightly stretched across the surface of the part; they want to crack and open up in order to make themselves more stable.

Second, the brightening agents and heavy metal stabilizers in most Electroless Nickel baths codeposit with the coatings producing defect nucleation sites. These are zones where the metal is locally stretched and weak; they are like nicks in the edge of a rubber band. Because of the stress in the coating, the weak zone tears and pores are formed.

CONCLUSION

To provide maximum corrosion protection, both phosphorus and contaminant content must be carefully controlled. This can only be obtained by proper bath formulation and by careful bath control.

GUIDE TO THE CORROSION RESISTANCE OF ELECTROLESS NICKEL

| ENVIRONMENT | CONCENTRATION WT. % | TEMPERATURE | | CORROSION RESISTANCE |
|-------------------------|------------------------|-------------|-----|-------------------------|
| | | °C | °F | |
| Acacia | 1 | 20 | 70 | A |
| Acetic Acid | 2-90 | 20 | 70 | C |
| Acetone | 100 | 54 | 130 | A |
| Aluminum Chloride | 41 | 20 | 70 | D |
| Aluminum Sulfate (Alum) | 5-27 | 20 | 70 | B |
| Ammonium Bicarbonate | 14 | 20 | 70 | B |
| Ammonium Chloride | 5-27 | 20 | 70 | B |
| Ammonium Hydroxide | 5-28 | 20 | 70 | C |
| Ammonium Nitrate | 5-66 | 20 | 70 | B |
| Ammonium Phosphate | 35 | 20 | 70 | B |
| Ammonium Sulfate | 43 | 20 | 70 | A |
| Amyl Alcohol | 100 | 20 | 70 | A |
| Amyl Chloride | 100 | 20 | 70 | A |
| Ascorbic Acid | 5 | 20 | 70 | B |
| Atmosphere, Industrial | -- | 20 | 70 | A |
| Atmosphere, Marine | -- | 20 | 70 | A |
| Atmosphere, Rural | -- | 20 | 70 | A |
| Barium Chloride | 2-40 | 20 | 70 | A |
| Barium Hydroxide | 2-50 | 60 | 140 | A |
| Beer | Product | Chilled | | A |
| Beet Sugar Liquor | Product | 20 | 70 | A |
| Benzene | 100 | 20 | 70 | A |
| Benzoic Acid | 1 | 20 | 70 | C |
| Benzyl Alcohol | 100 | 20 | 70 | A |
| Borax | 3 | 20 | 70 | B |
| Boric Acid | 1-5 | 20 | 70 | B |
| Bromine, Dry | 100 | 20 | 70 | A |
| Bromine, Wet | 100 | 20 | 70 | B |
| Butadiene | 100 | 26 | 80 | A |
| Butane | 100 | 26 | 80 | A |
| Butyl Alcohol | 100 | 20 | 70 | A |
| Brine, Oil Field | -- | 60 | 140 | A |
| Calcium Chloride | 40 | 20 | 70 | A |
| Calcium Nitrate | 50 | 20 | 70 | A |
| Calcium Hydroxide | 1 | 60 | 140 | A |
| Cane Sugar Liquor | 100 | 95 | 200 | A |
| Caprolactam | Product | 82 | 180 | A |
| Carbon Black | 20 | 20 | 70 | A |
| Carbon Dioxide, Dry | 100 | 400 | 750 | A |
| Carbon Dioxide, Wet | 100 | 20 | 70 | B |
| Carbon Disulfide | 100 | 20 | 70 | A |
| Carbon Tetrachloride | 100 | Boiling | | A |
| Chlorine, Dry | 100 | 20 | 70 | A |
| Chlorine, Wet | 100 | 20 | 70 | B |
| Chlorobenzene | 100 | 20 | 70 | A |
| Chloroform | 100 | 20 | 70 | A |
| Chloroform | 100 | Boiling | | B |
| Chrome Plating Solution | Standard | 20 | 70 | B |
| Chromic Acid | 2-100 | 20 | 70 | D |
| Citric Acid | 5-50 | 20 | 70 | C |
| Coffee | Product | Boiling | | A |
| Corn Syrup Liquor | Product | 20 | 70 | B |

GUIDE TO THE CORROSION RESISTANCE OF ELECTROLESS NICKEL

PAGE 2

| ENVIRONMENT | CONCENTRATION WT. % | TEMPERATURE | | CORROSION RESISTANCE |
|-------------------------|------------------------|-------------|------|-------------------------|
| | | °C | °F | |
| Copper Chloride | 5-40 | 20 | 70 | D |
| Copper Nitrate | 5 | 20 | 70 | B |
| Copper Plating Solution | Standard | 20 | 70 | A |
| Copper Sulfate | 5-30 | 20 | 70 | C |
| Cresylic Acid | 1-100 | 20 | 70 | A |
| Crude Oil | 100 | 20 | 70 | A |
| Detergent | 1 | 20 | 70 | A |
| Dextrin | 1 | 20 | 70 | A |
| Dichloroethene | 100 | 20 | 70 | A |
| Diethanolamine | 30 | 95 | 200 | A |
| EDTA | 1 | 20 | 70 | C |
| Ethyl Alcohol | 100 | 20 | 70 | A |
| Ethylene | 100 | 20 | 70 | A |
| Ethylene Dichloride | 100 | Boiling | | A |
| Ethylene Glycol | 100 | 20 | 70 | A |
| Fatty Acids | 100 | 20 | 70 | B |
| Ferric Chloride | 1-48 | 20 | 70 | D |
| Ferric Nitrate | 5 | 20 | 70 | D |
| Ferric Sulfate | 21 | 20 | 70 | D |
| Flue Gas, Oxidizing | -- | 540 | 1000 | A |
| Flue Gas, Reducing | -- | 260 | 500 | D |
| Fluoroboric Acid | 48 | 20 | 70 | D |
| Formaldehyde | 37 | 20 | 70 | B |
| Formic Acid | 10-88 | 20 | 70 | B |
| Fruit Juices | Product | 20 | 70 | A |
| Fuel Oil | 100 | 20 | 70 | A |
| Gasoline | 100 | 20 | 70 | A |
| Gin | Product | 20 | 70 | A |
| Glucose | 45 | 20 | 70 | A |
| Glycerine | 100 | 20 | 70 | A |
| Hydrochloric Acid | 1-36 | 20 | 70 | C |
| Hydrofluoric Acid | 2-49 | 20 | 20 | D |
| Hydrogen Chloride, Dry | 100 | 20 | 70 | A |
| Hydrogen Sulfide, Dry | 100 | 20 | 70 | A |
| Hydrogen Sulfide, Wet | 100 | 20 | 70 | A |
| Iodine | 0.1N | 20 | 70 | D |
| Isopropyl Alcohol | 100 | 20 | 70 | A |
| Jet Fuel | 100 | 20 | 70 | A |
| Kerosene | 100 | 20 | 70 | A |
| Lactic Acid | 10-50 | 20 | 70 | C |
| Lactic Acid | 85 | 20 | 70 | A |
| Lead Acetate | 35 | 20 | 70 | B |
| Lead Nitrate | 36 | 20 | 70 | A |
| Lemon Juice | Product | 20 | 70 | A |
| Linseed Oil | 100 | 20 | 70 | A |
| Lithium Chloride | 46 | 20 | 70 | A |

GUIDE TO THE CORROSION RESISTANCE OF ELECTROLESS NICKEL

PAGE 3

| ENVIRONMENT | CONCENTRATION WT. % | TEMPERATURE | | CORROSION RESISTANCE |
|------------------------|------------------------|-------------|-----|-------------------------|
| | | °C | °F | |
| Magnesium Chloride | 2-50 | 20 | 70 | A |
| Magnesium Hydroxide | 2-100 | 20 | 70 | A |
| Maleic Acid | 44 | 20 | 70 | A |
| Malic Acid | 10-50 | 20 | 70 | B |
| Mercurous Chloride | 1 | 20 | 70 | B |
| Methyl Alcohol | 100 | 20 | 70 | A |
| Methyl Cellulose | 10 | 20 | 70 | A |
| Methyl Chloride | 100 | 20 | 70 | C |
| Methyl Ethyl Ketone | 100 | 20 | 70 | A |
| Milk | Product | 20 | 70 | A |
| Mine Water, Acid | -- | 20 | 70 | B |
| Molasses, Raw | Product | 20 | 70 | A |
| Molasses, Raw | Product | 104 | 220 | B |
| Monoethanolamine | 20 | 95 | 200 | A |
| Naphtha | 100 | 20 | 70 | A |
| Naphthenic Acid | 100 | 20 | 70 | B |
| Nickel Chloride | 72 | 20 | 70 | A |
| Nickel Sulfate | 38 | 20 | 70 | C |
| Nitric Acid | 10-70 | 20 | 70 | D |
| Nitrobenzene | 100 | 20 | 70 | A |
| Oil, Petroleum | 100 | 20 | 70 | A |
| Oil, Mineral | 100 | 20 | 70 | A |
| Oil, Palm | 100 | 20 | 70 | A |
| Oil, Peanut | 100 | 20 | 70 | A |
| Oil, Vegetable | 100 | 20 | 70 | A |
| Oleic Acid | 100 | 20 | 70 | A |
| Oleum | 20 | 20 | 70 | D |
| Orange Juice | Product | 20 | 70 | A |
| Oxalic Acid | 10 | 20 | 70 | C |
| Palmitic Acid | 100 | 20 | 70 | C |
| Paraffin | 100 | Molten | | A |
| Perchloroethylene | 100 | 20 | 70 | A |
| Phenol | 25-100 | 95 | 200 | A |
| Phosphoric Acid | 10-85 | 20 | 70 | B |
| Phthalic Anhydride | 10 | 20 | 70 | A |
| Picric Acid | 1 | 20 | 70 | D |
| Polymers | 100 | 200 | 400 | A |
| Potassium Carbonate | 27 | 95 | 200 | A |
| Potassium Chloride | 25 | 20 | 70 | A |
| Potassium Ferricyanide | 5-25 | 20 | 70 | A |
| Potassium Hydroxide | 2-50 | 20 | 70 | A |
| Potassium Nitrate | 24 | 20 | 70 | A |
| Propane | 100 | 20 | 70 | A |
| Resins | 100 | 50 | 120 | A |
| Rochelle Salts | 35 | 20 | 70 | B |
| Rosin | 100 | Boiling | | A |
| Rum | Product | 20 | 70 | A |
| Soap Wash Liquor | Product | 95 | 200 | A |
| Sodium Bicarbonate | 2-14 | 20 | 70 | B |
| Sodium Carbonate | 18 | 20 | 70 | A |
| Sodium Chloride | 5-26 | 20 | 70 | A |

GUIDE TO THE CORROSION RESISTANCE OF ELECTROLESS NICKEL

PAGE 4

| <u>ENVIRONMENT</u> | <u>CONCENTRATION WT. %</u> | <u>TEMPERATURE</u> | | <u>CORROSION RESISTANCE</u> |
|---------------------|--------------------------------|--------------------|-----------|---------------------------------|
| | | <u>°C</u> | <u>°F</u> | |
| Sodium Cyanide | 5-10 | 20 | 70 | B |
| Sodium Hydroxide | 2-50 | 120 | 250 | A |
| Sodium Hypochlorite | 1-5 | 20 | 70 | A |
| Sodium Nitrate | 10 | 20 | 70 | A |
| Sodium Nitrite | 42 | 20 | 70 | B |
| Sodium Phosphate | 46 | 20 | 70 | A |
| Sodium Silicate | 10 | 20 | 70 | A |
| Sodium Sulfate | 31 | 20 | 70 | A |
| Sodium Sulfide | 14 | 20 | 70 | A |
| Soup | Product | 95 | 200 | A |
| Steam | -- | 430 | 800 | A |
| Steam Condensate | -- | 82 | 180 | A |
| Stearic Acid | 2 | 20 | 70 | A |
| Sugar Liquor | Product | 20 | 70 | A |
| Sulfuric Acid | 1-85 | 20 | 70 | C |
| Sulfuric Acid | 85-98 | 20 | 70 | D |
| Sulfurous Acid | 2-60 | 20 | 70 | D |
| Tall Oil | 100 | 20 | 70 | A |
| Tanning Solution | 100 | 20 | 70 | A |
| Thiourea | 8 | 20 | 70 | D |
| Toluene | 100 | 95 | 200 | A |
| Trichloroethylene | 100 | 95 | 200 | A |
| Turpentine | 100 | 20 | 70 | A |
| Urea | 58 | 20 | 70 | D |
| Varnish | 100 | 20 | 70 | A |
| Vinegar | Product | 20 | 70 | B |
| Vinyl Chloride | 100 | 38 | 100 | A |
| Vodka | Product | 20 | 70 | A |
| Water, Boiler Feed | -- | 200 | 400 | A |
| Water, Cooling | -- | 38 | 100 | A |
| Water, Deionized | -- | 82 | 180 | A |
| Water, Distilled | -- | 20 | 70 | A |
| Water, Fresh | -- | 20 | 70 | A |
| Water, Acid Mine | -- | 20 | 70 | C |
| Water, Sea | -- | 20 | 70 | A |
| Wine | Product | 20 | 70 | B |
| Whiskey | Product | 20 | 70 | A |
| Xylenes | 100 | 20 | 70 | A |
| Zinc Chloride | 5-10 | 20 | 70 | B |
| Zinc Nitrate | 35 | 20 | 70 | B |
| Zinc Sulfate | 20 | 20 | 70 | D |

NOTES:

1. Code: A = Satisfactory, corrosion rate generally less than 0.1 mpy ($2\frac{1}{2}$ $\mu\text{m}/\text{y}$).
B = Usually satisfactory, corrosion rate generally less than 0.5 mpy ($12\frac{1}{2}$ $\mu\text{m}/\text{y}$).
C = Sometimes useful, corrosion rate generally less than 1 mpy (25 $\mu\text{m}/\text{y}$).
D = Usually unsatisfactory for long term exposure, corrosion rate greater than 1 mpy (25 $\mu\text{m}/\text{y}$).
2. All solution concentrations are shown in percentage by weight in water except where otherwise indicated.
3. The information presented in this listing is as complete and accurate as possible at the time of publication. It is intended as a guide only, and not as an implied recommendation. Variations in environments and their contaminants as well as, processing techniques, can effect corrosion resistance and must be considered.

RND: js
April 10, 1981

Revised
December 2, 1982